

A STABILIZE ANGLE POSITION OF ARM ROBOT

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ABSTRACT

In modern industrial, there are many object of control system with use for driving special tools and materials transportation is arm robot system. Basically the operation of arm robot system is position control. DC motor is one of the most powerful machines it can be used for tracking the movement of an arm robot. But the problem is how to make a stable condition of the angle position of the arm robot. The answer is Position Control Design. So in this research I did to solve the problem. The control position of the arm robot system consists of DC motor, encoder and other devices. Analyzing the system we applied state feed back for stabilize inverter pendulum. "The Position of Arm Robot" control system is realized under digital signal processing controlling DC motor. That applied that system.

THE ARM ROBOT SYSTEM

The Arm Robot Angle Position Control

In our study case how can a feed back system control a arm robot position. The system as like picture in Fig. 2. The arm robot is derived by a DC motor.

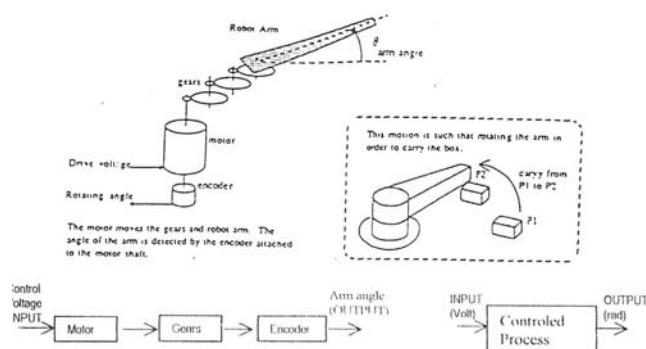


Fig.1 The Arm Robot

Physical Model Of DC Motor

In these control system, the variable being controlled is position. The position is measured by a encoder as sensor.

The Phisical model of the Arm Robot position control

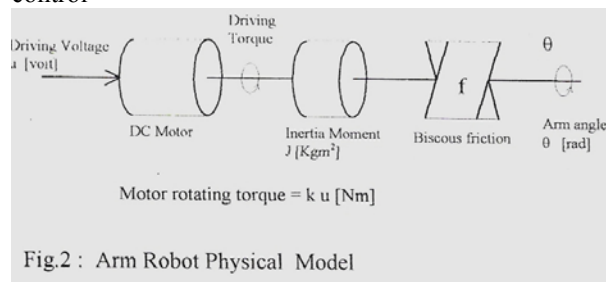


Fig.2 : Arm Robot Physical Model

Fig-2 Arm Robot Physical Model

Mathematical Model

From Physical model at Fig-3, It should be described more detail of the model as fig-4 below. And accordance with several theorem basically likes Kirchof, Newton Low and Dynamic equations We can construct mathematical model of the system.

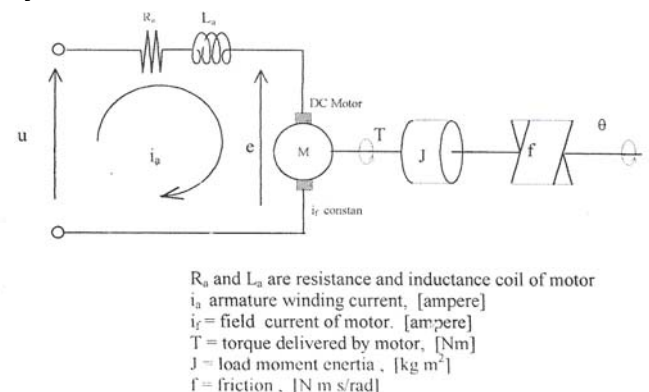


Fig-3 Electrical and Mechanical DC Motor

The torque T delivered by motor is proportional to armature current i_a and gap the air gap flux ψ . The air gap flux ψ proportional to field current i_f , it can be wrote as :

$$\psi = k_f i_f \quad (1)$$

k_f = constante field current

$$T = k_a i_a \quad (2)$$

k_a = constante armature current

where ψ = magnetic flux at air gap

By using $k = k_f i_f k_a$ it can be

$$T = k i_a \quad (3)$$

Because of flux constant so the voltage induced e_b is proportional to the angular velocity directly. And it can be wrote that:

$$e_b = k_b \frac{d\theta}{dt} \quad (4)$$

where k_b is a back emf constant.

The input voltage $u(t)$ is supplied by amplifier. It can find the differential equation for i_a :

$$L_a \frac{di_a}{dt} + R_a i_a + e = u \quad (5)$$

Torque T which be applied to the inertia moment and friction is produced by armatur current. It can be wrote as:

$$J \frac{d^2\theta}{dt^2} + f \frac{d\theta}{dt} = T = k i_a \quad (6)$$

In Laplace version we can write the equations 4,5 dan 6 as below:

$$k_b s \Theta(s) = E(s) \quad (7)$$

$$(L_a s + R_a) I_a(s) + E(s) = U(s) \quad (8)$$

$$(J s^2 + f s) \Theta(s) = T(s) = k I_a(s) \quad (9)$$

Accordance with the laplace equation 7,8 dan 9 we make a diagram block of the system. We can the system diagram block at Fig.4 as below:

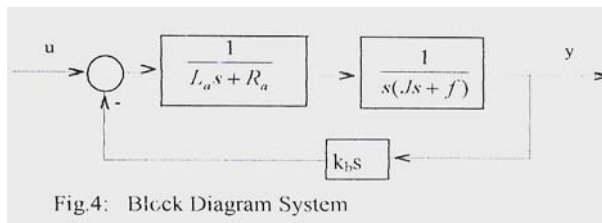


Fig.4: Block Diagram System

The transfer function of the system as:

$$\frac{\Theta(s)}{E(s)} = \frac{k}{s [L_a J s^2 + (L_a f + R_a J) s + R_a f + k k_b]} \quad (10)$$

Usually the inductance L_n is small and may be neglected. And as result the transfer function given by equation (10) reduces to:

$$\frac{\Theta(s)}{U(s)} = \frac{k_m}{s(T_m s + 1)} \quad (11)$$

The transfer function is second order and the system's block diagram of "Arm Robot" is :

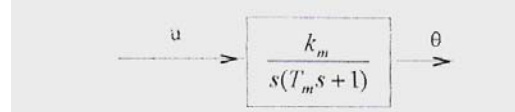


Fig.5: the arm robot open loop transfer function

Experimentally we can find the value of k_m and T_m

Measure k_m and T_m

In order to measure k_m and T_m the step function (voltage) is supplied to the system. We have already know mathematically an output of the system should be transient function:

$$\theta(t) = k_m \left(1 - e^{-\frac{t}{T_m}} \right) u(t) \quad (12)$$

Where, T_m = arm robot time constant [sec]
 k_m = value of $B(t = \infty)$ [rad/volt]

In our case for control position of arm robot we used a step function for input system, Based on the input step function it can be obtained the value output parameter in mathematically, let consider Equation 12.

Input step function $U(s) = 1$ and

$$\theta(t) = \frac{k_m}{T_m} (1 - e^{-\frac{t}{T_m}})$$

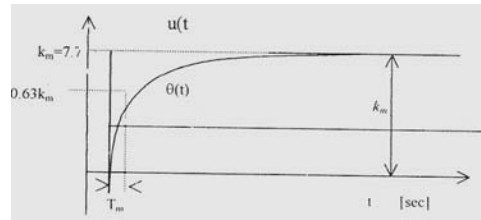
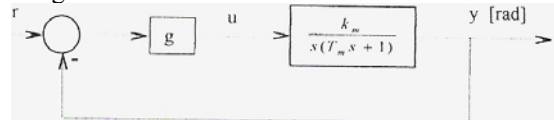


Fig-6 Open loop output response system With a input step function

In experiment it find $k_m = 7.7$ rad/sec and $T_m = 0.14$

Arm Robot Feedback control

The Arm robot position can be controlled by using a feed back control. One of that feed back as a Fig-8.



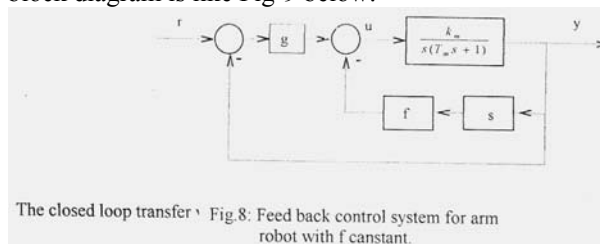
This block diagram is 2 order and it have 2 poles. We can find it's closed loop transfer function. The transfer function is:

$$\frac{Y(s)}{R(s)} = \frac{\frac{g}{T_m}}{s^2 + \frac{k_m}{T_m} s + \frac{g}{T_m}} \quad (13)$$

A position of poles should be determine a output response of the system. The best response is critically damped. Because the critically damped output response have a shortest time response (taster) and without any overshoot.

So to find the best response (critically damped) we have to chose which poles are suitable for our system. Poles of the closed loop transfer function should be consist of complex numbers.

Accordance with equation 12 we can change g parameter constant value. But unfortunately if we change g there only imaginary part of that poles can be changed and there no effect for real part. So to over come this problem it should suggest to change a block diagram with another. The a new system block diagram is like Fig-9 below:

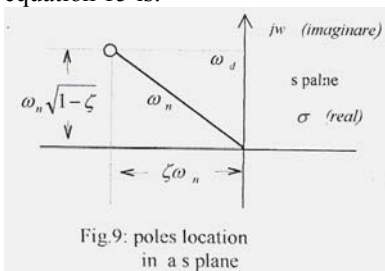


$$\frac{Y(s)}{R(s)} = \frac{\omega_n^2}{s^2 + \frac{1}{T_m}(1 + k_m f)s + \frac{k_m}{T_m}g} \quad (14)$$

This equation similar with

$$\frac{Y(s)}{R(s)} = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} \quad (15)$$

poles location for the transfer function accordance equation 15 is:



A $r(t)$ input step function will produce an output equation $y(t)$ as below:

$$y(t) = 1 - \frac{e^{-\zeta\omega_n t}}{\sqrt{1-\zeta^2}} \sin(\omega_d t + \tan^{-1}(\frac{\sqrt{1-\zeta^2}}{\zeta})) \quad (16)$$

ω_d is imaginary part of poles, and time constant of output response system τ is:

$$\tau = \frac{1}{\zeta\omega_n}$$

response of system. If we want to have time response more faster so it need that in mathematically ω_n more bigger in our system control design. But it have limitation accordance physical parameter value of the arm robot. And by using the equation 13 we can evaluate or change both of poles part are

real and imaginary in order to get best response of the system mathematically.

In order to get a critically damped output response we should chose the "damping ratio" ζ is 0.8.

As we know in experiment we have already find

$$k_m = 7.7 \text{ rad/volt} \quad \text{and} \quad T_m = 0.14 \text{ sec}$$

By using $g=1.0$ We can find the value of ω_n and feedback parameter f from equation 13 and 14 as below:

$$\omega_n = \sqrt{\frac{k_m}{T_m}g} = \sqrt{\frac{7.7}{0.14}} = 7.3485 \quad \text{and}$$

$$2\zeta\omega_n = \frac{1}{T_m}(1 + k_m f)$$

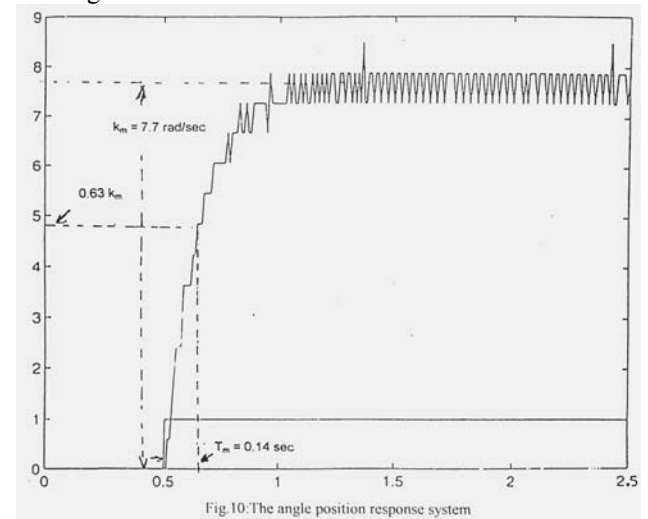
$$\begin{aligned} \text{And then} \quad f &= \frac{2\zeta\omega_n T_m - 1}{k_m} \\ &= \frac{(2)(0.8)(7.3485)(0.14) - 1}{7.7} \\ f &= 0.084 \end{aligned}$$

Beside of damping ratio and frequency method an we also find a best output response by replacement of poles in try and error method.

Finally we find a curve graphic of output response for:

$$\begin{aligned} k_m &= 7.7 \text{ [rad/second]} \\ T_m &= 0.14 \text{ [second]} \\ G &= 1.0 \\ F &= 0.084 \end{aligned}$$

As a fig.10 below :



SUMMARY

- Within non overshoot output range condition, we find that the minimal value of time constant response system 0.14 second.
- Cause of gear box hysteresis, so the angle output system have a small vibration.
- The limitation of DC motor input voltage will determine a speed response of the system